
EEE321 Electromagnetic Fields and Waves

Prof. Dr. Hasan Hüseyin BALIK

(13th Week)

Outline

- Nonuniform plane waves
- Total reflection
- Reflection and refraction at the surface of a good conductor

Nonuniform Plane Waves

- In a plane wave, the equiphase surfaces are planes.
- In a uniform plane wave, the amplitude is uniform throughout any given plane equiphase surface
- In a ununiform plane wave, the equiphase surface are still uniform but the amplitude over a given equiphase is not uniform.

- With nonuniform plane waves, we can still wirite that

$$\mathbf{E} = \mathbf{E}_m \exp j(\omega t - \mathbf{k} \cdot \mathbf{r}), \quad (31-2)$$

$$\mathbf{H} = \mathbf{H}_m \exp j(\omega t - \mathbf{k} \cdot \mathbf{r}), \quad (31-3)$$

- Where the amplitudes \mathbf{E}_m , \mathbf{H}_m may be complex. The wave vector then has the form

$$\mathbf{k} = \boldsymbol{\beta} - j\boldsymbol{\alpha}, \quad (31-4)$$

- Where the two real vectors $\boldsymbol{\alpha}$ and $\boldsymbol{\beta}$ points in different direction

- Then

$$\mathbf{E} = \mathbf{E}_m \exp(-\boldsymbol{\alpha} \cdot \mathbf{r}) \exp j(\omega t - \boldsymbol{\beta} \cdot \mathbf{r}), \quad (31-5)$$

$$\mathbf{H} = \mathbf{H}_m \exp(-\boldsymbol{\alpha} \cdot \mathbf{r}) \exp j(\omega t - \boldsymbol{\beta} \cdot \mathbf{r}). \quad (31-6)$$

- Above equations define a wave that propagates in the positive direction of the vector $\boldsymbol{\beta}$ at the phase velocity

$$v = \frac{\omega}{\beta} \quad (31-7) \quad \text{and whose wavelength is}$$

$$\lambda = \frac{2\pi}{\beta}, \quad \text{hence} \quad \beta = \frac{1}{\lambda}. \quad (31-8)$$

- The amplitude of the wave decreases exponentially in the positive direction of $\boldsymbol{\alpha}$ and the attenuation distance δ , over which the amplitude decreases by the factor of e , given by

$$\delta = \frac{1}{\alpha}. \quad (31-9)$$

- Expression of \mathbf{E} in the general wave equation

$$k^2 = (\boldsymbol{\beta} - j\boldsymbol{\alpha})^2 = \beta^2 - \alpha^2 - 2j\boldsymbol{\alpha} \cdot \boldsymbol{\beta} = \omega^2 \epsilon \mu - j\omega \sigma \mu, \quad (31-10)$$

$$\beta^2 - \alpha^2 = \omega^2 \epsilon \mu, \quad 2\boldsymbol{\alpha} \cdot \boldsymbol{\beta} = \omega \sigma \mu, \quad (31-11)$$

Complex Angle

- From Euler formulation $\cos A + j \sin A = e^{jA}$ can be used. By extension A can be any complex number. Then

$$\sin A = \frac{\exp jA - \exp(-jA)}{2j}, \quad \cos A = \frac{\exp jA + \exp(-jA)}{2}. \quad (31-14)$$

- Clearly $\sin A$ can now be any complex number. The same applies to $\cos A$. As with real angles

$$\sin^2 A + \cos^2 A = 1. \quad (31-15)$$

$$\sin(A + 2\pi) = \sin A, \quad \cos(A + 2\pi) = \cos A. \quad (31-16)$$

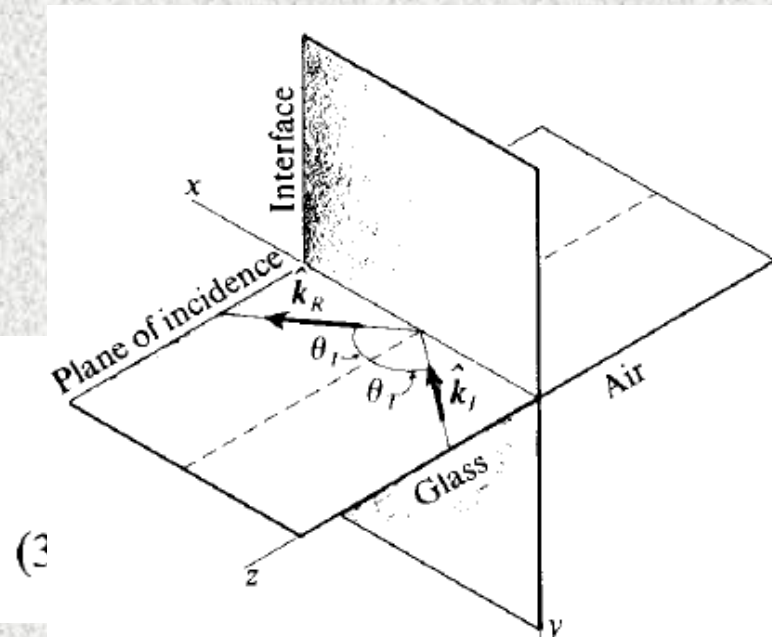
Total Reflection

- Total reflection leads to a value of $\sin \theta_T > 1$, then θ_T is complex. Snell's law and Fresnel's equations still apply
- Critical angle of incidence, for which $\theta_T = 90$ is given by

$$\sin \theta_{Ic} = \frac{n_2}{n_1}. \quad (31-17)$$

- At angles $\theta_I > \theta_{Ic}$, $\sin \theta_T$ is greater than unity than θ_T is complex. Then the wave is totally reflected.
- This phenomenon is independent of the orientation of the **E** vector in the incident wave
- Total reflection has many uses (i.e optical wave guides)
- Set $\theta_T = a + jb$, then

$$\begin{aligned} \sin \theta_T &= \frac{\exp j(a + jb) - \exp (-j)(a + jb)}{2j} \\ &= \frac{\exp ja \exp (-b) - \exp (-ja) \exp b}{2j}. \end{aligned}$$



- Since this quantity is real, a must be equal to $\pi/2$ and

$$\sin \theta_T = \frac{\exp b + \exp(-b)}{2} = \cosh b. \quad (31-20)$$

$$\theta_T = \frac{\pi}{2} + jb. \quad (31-21)$$

- Then

$$\begin{aligned} \cos \theta_T &= \frac{\exp j(a + jb) + \exp(-j)(a + jb)}{2} \\ &= \frac{j[\exp(-b) - \exp b]}{2} = -j \sinh b. \end{aligned} \quad (31-22)$$

$$\cos \theta_T = (1 - \sin^2 \theta_T)^{1/2} = -j(\sin^2 \theta_T - 1)^{1/2}. \quad (31-23)$$

- The incident, reflected and transmitted waves are the same form as defined in Snell's law:

$$E_I = E_{Im} \exp j[\omega t - k_1(x \sin \theta_I - z \cos \theta_I)], \quad (31-24)$$

$$E_R = E_{Rm} \exp j[\omega t - k_1(x \sin \theta_I + z \cos \theta_I)], \quad (31-25)$$

$$E_T = E_{Tm} \exp j[\omega t - k_2(x \sin \theta_T - z \cos \theta_T)]. \quad (31-26)$$

The Reflected Wave

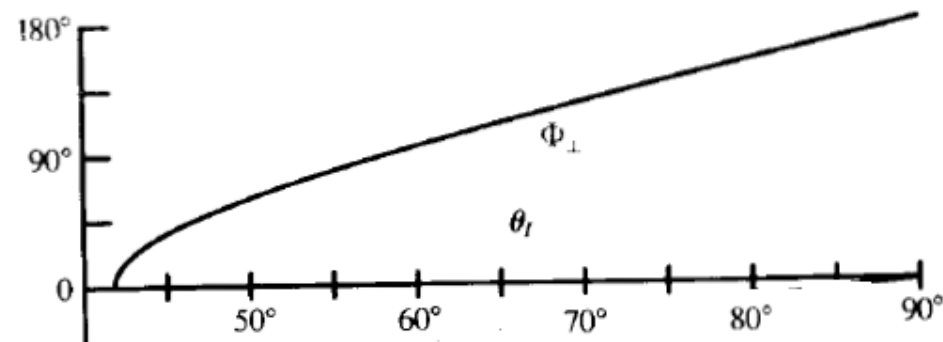
- Applying Fresnell's equations, we find that

$$\left(\frac{E_{Rm}}{E_{Im}}\right)_{\perp} = \frac{(n_1/n_2) \cos \theta_I + j(\sin^2 \theta_T - 1)^{1/2}}{(n_1/n_2) \cos \theta_I - j(\sin^2 \theta_T - 1)^{1/2}} = \exp j\Phi_{\perp}, \quad (31-27)$$

- Where

$$\Phi_{\perp} = 2 \arctan \frac{(\sin^2 \theta_T - 1)^{1/2}}{(n_1/n_2) \cos \theta_I}. \quad (31-28)$$

- This is the phase of the reflected wave with respect to the incident wave at any point in the interface. The reflected wave leads the incident wave for this polarisation
- Since total reflection is lossless, the incident and reflected waves are of the same amplitude



The Transmitted Wave

- The vector wave number for the transmitted wave is

$$\mathbf{k}_T = \boldsymbol{\beta}_T - j\boldsymbol{\alpha}_T = k_2(\sin \theta_T \hat{\mathbf{x}} - \cos \theta_T \hat{\mathbf{z}}) \quad (31-29)$$

$$= k_2(\sin \theta_T \hat{\mathbf{x}} + j \sinh b \hat{\mathbf{z}}). \quad (31-30)$$

- This term show that the wave travels in the positive x direction and attenuation in the negative z direction because b is positive.
- The attenuation distance in the direction perpendicular to the interface is

$$\delta_z = \frac{1}{k_2 \sinh b} = \frac{\lambda_0}{n_2 \sinh b} = \frac{\lambda_0}{2\pi n_2 \sinh b} = \frac{\lambda_2}{2\pi \sinh b}. \quad (31-31)$$

- Applying Fresnell's equations

$$\left(\frac{E_{Tm}}{E_{Im}} \right)_{\perp} = \frac{2 \cos \theta_I}{\cos \theta_I - j(n_2/n_1)(\sin^2 \theta_T - 1)^{1/2}} \quad (31-32)$$

$$= \frac{2 \cos \theta_I}{[\cos^2 \theta_I + (n_2/n_1)^2(\sin^2 \theta_T - 1)]^{1/2}} \exp j \frac{\Phi_{\perp}}{2} \quad (31-33)$$

$$= \frac{2 \cos \theta_I}{[1 - (n_2/n_1)^2]^{1/2}} \exp j \frac{\Phi_{\perp}}{2}. \quad (31-34)$$

- Let us calculate \mathbf{H}_T . Since the transmitted wave is not uniform, \mathbf{H}_T is not transverse. So

$$\mathbf{H}_T = \frac{\mathbf{k}_T \times \mathbf{E}_T}{\omega \mu_2} = \frac{\mathbf{k}_T \times \mathbf{E}_T}{Z_2 k_2} = \frac{\mathbf{k}_T \times E_T \hat{\mathbf{y}}}{Z_2 k_2} \quad (31-35)$$

$$= \frac{(\sin \theta_T \hat{\mathbf{x}} - \cos \theta_T \hat{\mathbf{z}}) \times E_T \hat{\mathbf{y}}}{Z_2} = \frac{(\cos \theta_T \hat{\mathbf{x}} + \sin \theta_T \hat{\mathbf{z}}) E_T}{Z_2}. \quad (31-36)$$

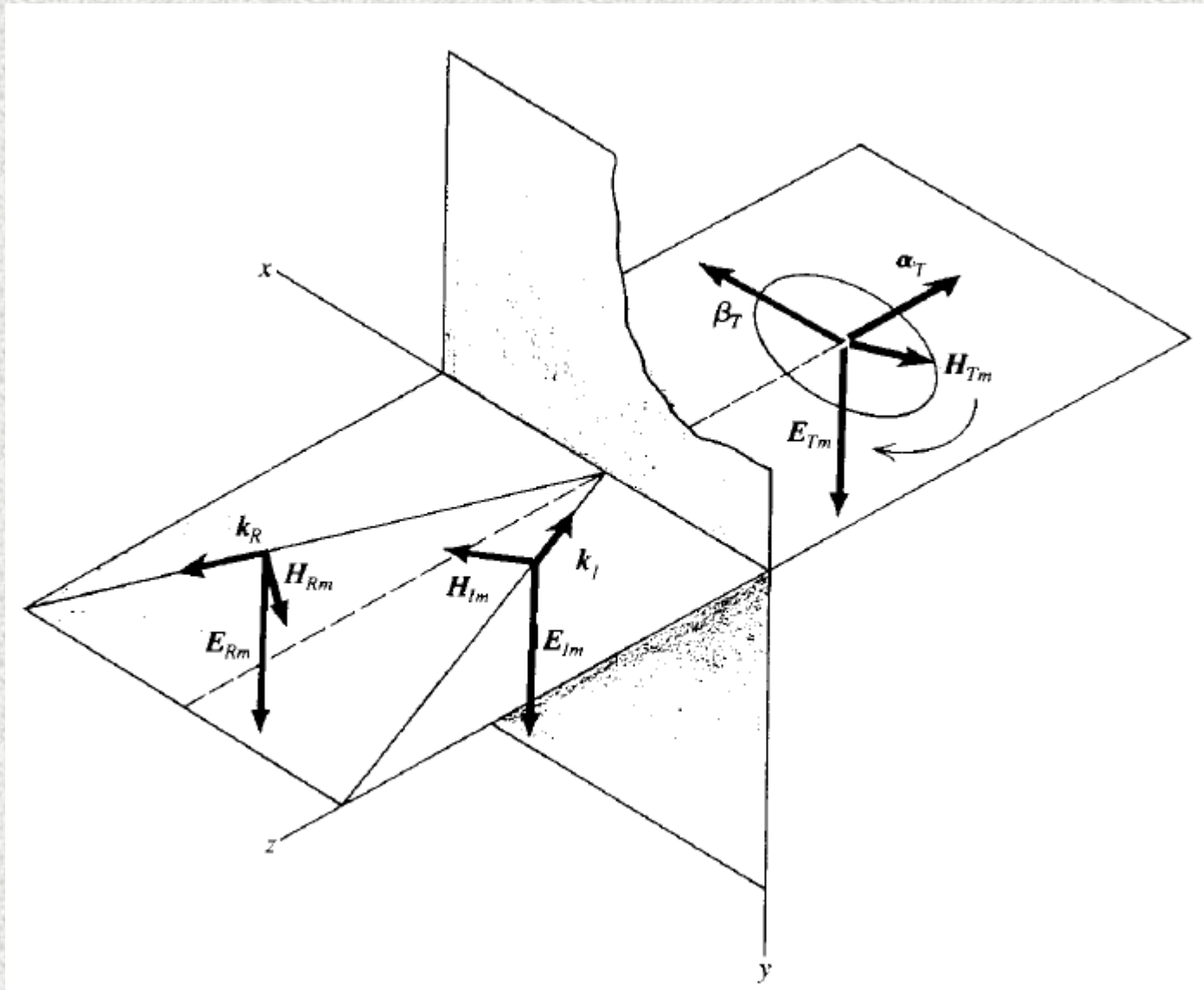
- Then $H_{Tmx} = \frac{E_{Tm}}{Z_2} \cos \theta_T, \quad H_{Tmz} = \frac{E_{Tm}}{Z_2} \sin \theta_T. \quad (31-37)$

- Since $H_{Tm} = \frac{E_{Tm}}{Z_2}, \quad (31-38)$

- Then

$$H_{Tmx} = H_{Tm} \cos \theta_T, \quad H_{Tmz} = H_{Tm} \sin \theta_T, \quad (31-39)$$

- Since $\sin \theta_T$ is real and positive while $\cos \theta_T$ is imaginary and negative the \mathbf{HT} vector rotates at the angular velocity ω as in figure



Reflection and Refraction at the Surface of a Good Conductor

- Consider the second medium is a good conductor as given in the figures.
- We may write that

$$\mathbf{E}_I = \mathbf{E}_{Im} \exp j(\omega t - k_1 x \sin \theta_I + k_1 z \cos \theta_I),$$

$$\mathbf{E}_R = \mathbf{E}_{Rm} \exp j(\omega t - k_1 x \sin \theta_I - k_1 z \cos \theta_I),$$

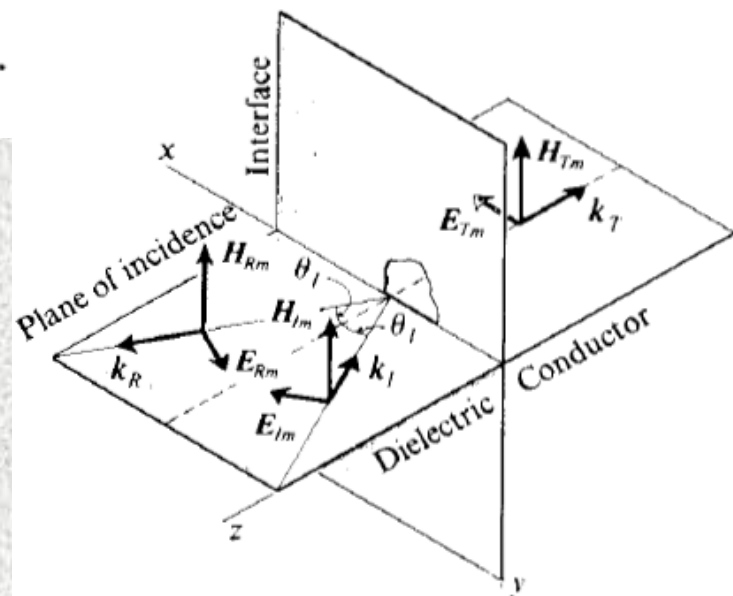
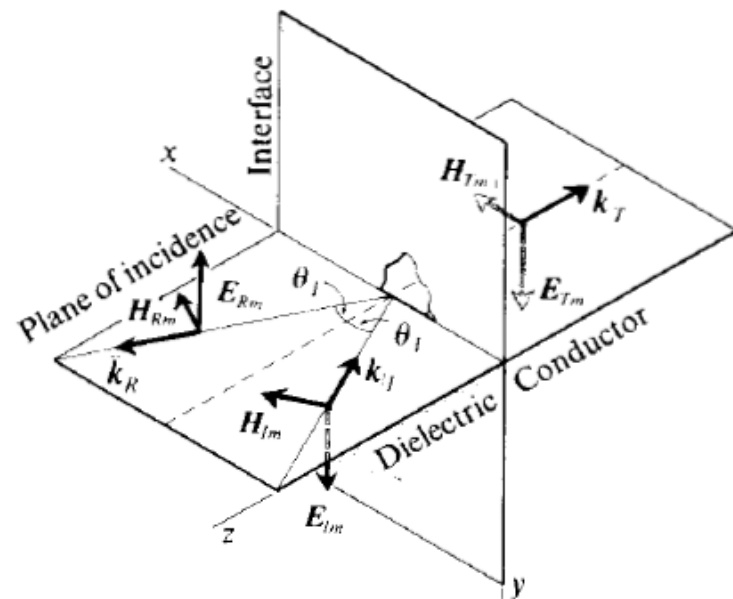
$$\mathbf{E}_T = \mathbf{E}_{Tm} \exp j(\omega t - k_1 x \sin \theta_I + k_2 z \cos \theta_T)$$

$$= \mathbf{E}_{Tm} \exp j \left\{ \omega t - k_1 x \sin \theta_I \pm k_2 z \left[1 - \left(\frac{n_1}{n_2} \right)^2 \sin^2 \theta_I \right]^{1/2} \right\}.$$

- From the definition

$$\frac{n_1}{n_2} = \frac{k_1}{k_2} = \frac{\omega(\epsilon_1 \mu_1)^{1/2} \delta}{1 - j} \quad (32-5)$$

$$= \frac{\delta}{(1 - j)\lambda_1}. \quad (32-6)$$



- We shall assume that

$$\frac{\delta}{2^{1/2}\lambda_1} \ll 1 \quad \text{or that} \quad \left| \frac{n_1}{n_2} \right| \ll 1. \quad (32-7)$$

- Then the expression in bracket in \mathbf{E}_T equation is approximately equal to unity. Then

$$\mathbf{E}_T = \mathbf{E}_{Tm} \exp j \left(\omega t - k_1 x \sin \theta_I \pm \frac{(1-j)z}{\delta} \right) \quad (32-8)$$

$$= \mathbf{E}_{Tm} \exp \left[j \left(\omega t - k_1 x \sin \theta_I \right) \pm \frac{(1+j)z}{\delta} \right]. \quad (32-9)$$

- For reflection from a good conductor

$$\cos \theta_T = + \left[1 - \left(\frac{n_1}{n_2} \right)^2 \sin^2 \theta_I \right]^{1/2} \approx 1, \quad \theta_T \approx 0. \quad (32-10)$$

$$\mathbf{E}_T \approx \mathbf{E}_{Tm} \exp \left[j \left(\omega t - k_1 x \sin \theta_I + \frac{z}{\delta} \right) + \frac{z}{\delta} \right]. \quad \mathbf{E}_T \approx \mathbf{E}_{Tm} \exp \left[j \left(\omega t + \frac{z}{\delta} \right) + \frac{z}{\delta} \right], \quad (32-13)$$

- The transmitted wave propagates into the conductor along the normal to the interface, whatever the angle of incidence, Also the amplitude decreases by the factor of e over one skin depth

E Normal to the Plane of Incidence

- From the Fresnell's equation with $\left|\frac{n_1}{n_2}\right| \ll 1$,

$$\left(\frac{E_{Rm}}{E_{Im}}\right)_{\perp} = \frac{(n_1/n_2) \cos \theta_I - \cos \theta_T}{(n_1/n_2) \cos \theta_I + \cos \theta_T} \approx -1 \quad (32-14)$$

- And from the fact that $\cos \theta_T \cong 1$,

$$\left(\frac{E_{Tm}}{E_{Im}}\right)_{\perp} = \frac{2(n_1/n_2) \cos \theta_I}{(n_1/n_2) \cos \theta_I + \cos \theta_T} \approx 2\frac{n_1}{n_2} \cos \theta_I \approx 0, \quad (32-15)$$

- At the surface of dielectric such that $n_2 \gg n_1$ one also has that

$$\left(\frac{E_{Rm}}{E_{Im}}\right)_{\perp} \approx -1, \quad \left(\frac{E_{Tm}}{E_{Im}}\right)_{\perp} \approx 0. \quad (32-16)$$

E Normal to the Plane of Incidence

- From Fresnell's equation

$$\begin{aligned}\left(\frac{E_{Rm}}{E_{Im}}\right)_{\parallel} &= \frac{(n_1/n_2) \cos \theta_T - \cos \theta_I}{(n_1/n_2) \cos \theta_T + \cos \theta_I} \\ &\approx \frac{(n_1/n_2) - \cos \theta_I}{(n_1/n_2) + \cos \theta_I} \approx -1.\end{aligned}\quad (32-17)$$

$$\left(\frac{E_{Tm}}{E_{Im}}\right)_{\parallel} = \frac{2(n_1/n_2) \cos \theta_I}{\cos \theta_I + (n_1/n_2) \cos \theta_T} \quad (32-18)$$

$$\approx \frac{2n_1}{n_2} = \frac{2n_1\delta}{1-j} = n_1\delta(1+j). \quad (32-19)$$

- Above approximations are not valid at grazing incidence, where θ_I is close to 90° .